

Developing and Characterizing Green Sorption Media for Nutrient Removal in an Innovative Septic Tank Underground Drainfield

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ABSTRACT

Growing worldwide concerns of nitrates and phosphorus in ground water led to research efforts directed towards developing a sorption media for a septic tank drainfield. Extensive research has been conducted in the past few decades, in order to find suitable media for denitrification with high selectivity towards nitrogen and phosphorus simultaneously. To explore a new design of septic tank underground drainfield with cost-effective, reliable, and longer life expectancy features, material characterization, packed bed column experiments, batch isotherm identification and microcosm study were collectively conducted and presented together in this paper so as to illuminate the potential of a suite of new material mixes. After initial literature review and multi-criteria decision making process, one of the columns was packed with tire crumb, saw dust and sand while the other column was packed with tire crumb, paper and sand. Under the hydraulic retention time (HRT) of 24 hours, samples illustrated treatment efficiencies of greater than 90% for both the columns for all pollutants of concerns. The batch adsorption isotherm data was fitted in the Langmuir isotherm and Freundlich isotherm models, and adsorption capacity for phosphorus was found to be 34.4 mg g⁻¹ Langmuir isotherm. A microcosm of the septic tank underground drainfield was built with one of the recipes applied in the column test as a continuous system dosed with synthetic wastewater. Under the HRT of 72 hours, samples from the microcosm physical model illustrated more than 80% of removal efficiency for nitrates and phosphorus. Additionally, with the aid of the isotherm tests, the life expectancy of the proposed sorption media in the microcosm physical model was estimated to be around 63 years for phosphorus sorption. Overall, the results indicate that the green sorption media investigated (i.e. “Black and GoldTM Nugget Mix”) has the potential for removal of nutrient flux and exhibit high potential of in full-scale field applications.

Keywords: Nutrient removal, Septic tank, Green sorption media, Sustainability Science

INTRODUCTION

Nitrate in drinking water system usually originates from fertilizers or from animal or human wastes. Nitrate concentrations in the natural water system tend to be highest in areas of intensive agriculture or where there are many septic systems. High nitrogen and phosphorus content in the water body has impeded water reuse potential and impacted ecosystem integrity and human health. Nitrate (NO_3^-) may be toxic and can cause human health problem such as methemoglobinemia, liver damage and possible cancers (WHO, 2006). Phosphorus (P) may trigger the eutrophication issues in fresh water bodies, which could result in toxic algae and endanger the source of drinking waters eventually (ESA, 2000). On the other hand, when urban regions gradually expand due to regional development, centralized sewage collection, treatment, and disposal is often unavailable for both geographic and economic reasons. Thus, decentralized or on-site wastewater treatment systems (OWTS) may be necessary to protect public health. Nation wide, wastewater effluent from OWTS can represent a large fraction of nutrient loads to groundwater aquifers, however.

In the modern era, OWTS also referred as septic system primarily includes a septic tank and soil adsorption field or drainfield also known as subsurface wastewater infiltration systems (SWIS). Drainfields are located in permeable, unsaturated natural soil or imported fill material so wastewater can infiltrate and percolate through the underlying soil to the ground water thereby treating itself through a variety of physical, chemical, and microbiological processes. However, the nitrate ion (NO_3^-) and soil are negatively charged, and so the NO_3^- ion is not bound to the soil. Therefore, nitrate ions move freely with the soil solution and are readily leachable. Nitrogen, particularly nitrates, easily moves from terrestrial ecosystems into surface and groundwater, including lakes, streams, rivers, and estuaries (Baker, 1992; Kahl et al., 1993;

Peterjohn et al., 1996). Two important processes that result in the transformation of nitrate are nitrification and denitrification. Nitrification is a process in which ammonium is oxidized and denitrification is a process in which nitrate is reduced back to nitrogen gas before escaping into the air. However, only denitrification that is a microbiologically mediated process occurring under anaerobic (oxygen depleted) conditions can result in the permanent removal of nitrate. Approximately, 55-85% of the nitrogen that enters the septic tank is available to ground water mainly in the form of nitrates (Stoltz and Reneau, 1998). Based on recent Florida research data, a family of four will discharge 11.36 Kg (25 pounds) of nitrogen (measured in the form of nitrates) per year into the drainfield of a conventional onsite sewage treatment and disposal system (Florida Department of Health, 2004).

Nitrates are the primary pollutants of concern in this research. The main risks are in “Blue baby” syndrome and suspected carcinogenic effect of nitrates on humans, and the nutrient enrichment of receiving waters. It has regulatory health limits in the US of maximum contamination level (MCL) of 10 mg-N L^{-1} . A septic tank with a conventional drainfield does not typically remove nitrogen in the form of nitrates since it is very soluble and does not sorb well to soil components during infiltration (Spalding and Kitchen, 1988). The use of different sorption media in septic tank drainfields turns out to be an appealing engineering approach in dealing with the increasing trend of higher nitrate concentrations that is expected to continue in the surface and groundwater systems. Besides, the use of the sorption media for denitrification rather than traditional gravel-filled drainfield for handling the effluents from the septic tank system would become a new focus in rural communities. Large-scale implementation with different sorption media to remove nutrients will be popular in the future (Mothersill et al., 2000; Birch et al., 2005).

It is believed that functionalized sorption media might have a better ion exchange capacity to support adsorption/desorption capacity. The aim of this paper is to screen sorption media via a thorough literature review, characterize the selected sorption media, and examine their sorption capacity for nutrient removal using column study, isotherm tests and microcosm assessment in support of the new underground drainfield design as an integral part of modern septic tank system. Pollutants of concern include nitrates, ammonia, total nitrogen, ortho-phosphorus, total phosphorus and BOD. Sorption media of interest include but are not limited to tire crumb, tree bark, wood chips, sawdust, paper (newspaper), alfalfa, mulch, cotton, wheat straw and sulfur/limestone. Two recipes with mixed sorption media were selected in the end of the initial literature study for columns study. At the end of the column study, the recipe including sand, tire crumb and sawdust was further used to estimate the sorption life of the media mix and also as a media mix for the design of microcosm physical model. The descriptions in the following sections start with investigating the material characterization then perform the column study, batch isotherm tests and end up with the assessment of microcosm physical model for further field implementation.

Literature review

Sorption Media Used for Nitrogen Species Removal

Many researchers had tried to remove nitrogen species by using sorption media. Kim et al., (2000) used different kinds of sorption media, such as alfalfa, mulch compost, newspaper, sawdust, wheat straw, wood chips for nitrate removal from storm water runoff. They found that alfalfa and newspaper had 100% nitrate removal efficiency but mulch compost had 60% nitrate removal efficiency. They also found that sawdust, wheat straw and wood chips had good removal efficiency (>95%), but wood chips showed consistently better performance in nitrate

removal over sawdust. From their experiment, it could be concluded that all of these were electron donors and good carbon sources for promoting denitrification. They suggested that increasing the retention time may gain better removal efficiency. Kim et al. (2000) also found that soil could only remove 7% to 10% of nitrate due to its anionic form.

Güngör and Ünlü (2005) conducted nitrate and nitrite removal experiment by using only three types of soils, including sandy clay loam (SCL), loamy sand (LS) and sandy loam (SM). They found significant nitrate and nitrite removal (i.e., over 90%). Hsieh and Davis (2005) found that mulch was very effective in removing nitrate, unlike sand. But they had not gained good ammonia removal efficiency by using mulch. They concluded that soil with higher silt/clay and cation (Mg/Ca/K) contents might be very effective in nutrient removal. They concluded that coarse media might not be able to retain the nutrient in repetitive loading due to small surface area so that sand should not be used.

Darbi et al., (2002) used sulfur and limestone for nitrate removal from potable water. In their experiment, sulfur was used as an electron donor and limestone was used to maintain the pH. They found that the optimum mixing ratio of sulfur and limestone is 1:1 for nitrate removal (i.e., about 98% nitrate removal was observed). They also suggested that increasing the retention time may obtain higher nitrate removal efficiency. Lisi et al. (2004) tried to use granulated tire for the removal of nitrate. They found 48.000 g of tire crumb can remove 16.2 g of NO_3^- -N. Sengupta and Ergas (2006) did an experiment to remove nitrate from wastewater by using marble chips, limestone and oyster shell. Their experiment gave some significant outcomes about using those solids as sorption media. They found that oyster shell (almost 98% CaCO_3) and limestone could remove 80% and 56% of nitrate, respectively. The pH and alkalinity were higher in testing using oyster shell rather than limestone and marble chips. Oyster shell was very much efficient to

reduce nitrite accumulation and dissolved oxygen (DO) did not work as a denitrification inhibitor when oyster shell was used as a sorption media. From these findings, it can be concluded that oyster shell is much more effective than limestone or marble chips for removing nitrate. Oyster shell can also be a good candidate for controlling the pH that is sensitive for denitrification.

Savage and Tyrrel (2005) used wood mulch, compost, soil, broken brick and polystyrene packaging for removal of $\text{NH}_3\text{-N}$ from compost leachate. They reached in a conclusion that wood mulch (75%) and compost (55%) had better removal efficiency for $\text{NH}_3\text{-N}$ than other media and polystyrene was the least capable one to remove $\text{NH}_3\text{-N}$. Soil and broken brick could remove 38% and 35% of $\text{NH}_3\text{-N}$, respectively. All these media had the same capability to remove BOD_5 by microbial oxidation process. The research group found that compost and wood mulch had a tendency to increase the pH. They concluded that specific surface area, void space, permeability, and adsorption capacity might influence the removal efficiency.

Sorption Media Used for Phosphorus Species Removal

Phosphorus removal from storm water is both precipitation and adsorption processes due to chemical reaction. As phosphorus has enormous effect on aquatic ecosystem, researchers have been trying to discover an economically feasible removal procedure. Some functionalized sorption media that can be used for phosphorus removal are sand rich with Fe, Ca or Mg, gravel, limestone, shale, light weight aggregates (LWA), zeolite (natural mineral or artificially produced alumino silicates), pelleted clay (along or in combination with soils), opaka (a siliceous sedimentary rock), pumice (natural porous mineral), wollastonite (a calcium metasilicate), fly ash, blast furnace slag (BFGS – a porous non-metallic co-product in iron industry), alum, goethite (a hydrous ferric oxide), hematite (a mineral form of iron(III) oxide), dolomite and calcite (Korkusuz, 2007).

DeBusk et al. (1997) used sand (with quartz), fresh organic (peat) soil, crushed lime rock (2.5 cm nominal size) and wollastonite (a mine containing calcium metasilicate plus ferrous metasilicate) to remove phosphorus (P), nickel (Ni) and cadmium (Cd) from storm water. They found that wollastonite had very good removal efficiency for their targeted contaminants. Wallastonite could remove about 87.8% P, 97.7% Cd and 80.3% Ni. On the other hand, limerock, peat and sand could remove 41.4%, 44%, and 41.4% P respectively. It can be concluded that wallastonite is very effective in phosphorus removal because it contains calcium and ferrous ions. Calcium and ferrous ions can remove phosphorus by precipitation reaction or adsorption.

Hsieh and Davis (2005) found good total phosphorus (TP) removal (about 41% to 48%) by sand and concluded that it might happen due to simple adsorption or complex sorption/precipitation processes. They found that mulch was not a good candidate for TP removal. This research group concluded that TP removal was highly variable and it might be related to properties of sorption media used and flow pattern of nutrient laden water through the sorption media. Again, organic matter could also accelerate TP removal up to 93%.

Richman (1997) found that compost had good removal efficiency for 90% solids, 85% oil and greases and 90% heavy metals. Clark and Pitt (2001) tried to remove contaminants in aerobic and anaerobic conditions from storm water runoff by using activated carbon, peat moss, compost and sand. They found good phosphorus removal efficiency by all four media in both conditions. They also found no desorption condition in their system for phosphorus. But they observed that sorption was better and leaching was lesser in aerobic condition for compost. Forbes et al. (2005) used lightweight expanded shale and masonry sand for the removal of

phosphorus. They summarized that sand is a poor candidate for retaining phosphorus and expanded shale has greater removal efficiency due to its larger surface area.

Tables 1-4 summarize all the sorption media used by different researchers to remove nutrient (both nitrogen and phosphorus species) from storm water and wastewater. For removing nitrogen and phosphorus from storm water or wastewater, these filtration media can be further classified based on the derivation from: 1) plants or processed from components of plants; 2) sand and clay; 3) minerals; and 4) waste materials that may be recycled from the society. The mixture with the water material in the particularly

Table 1: Sorption media derived from plants or processed from components of plants used to remove nutrients from storm water or wastewater

| No. | Sorption media | Additional environmental benefits in terms of removal | Physical/Chemical Properties | References |
|-----|--|---|---|--|
| 1 | Alfalfa | 100% NO ₃ -N removal; | D<4mm | Kim et al.(2000) |
| 2 | Leaf mulch compost/ Hardwood mulch/Wood compost | Copper , Cadmium, Lead, Zinc, 1, 3 dichlorobenzene (DCB), | Silver maple, Norway maple, Red oak and Cherry mulch (Ash 10.90%, 44.12% C, 5.86% H, 0.63% N, 0.16% S, 38.33% O), size 4760 micron, | Ray et al. (2006) |
| | | 60% NO ₃ -N removal; | D<2mm | Kim et al.(2000) |
| | | Oil & greases (85% removed), heavy metals (90% removed), | Maple & elm leaf compost | Richman (1997) |
| | | Lead | | Hsieh & Davis (2005) |
| 3 | Sawdust | | 30% sawdust Wall structure, Monterey pine (Pinus Radiata D. Don) sawdust, | Schipper et al. (2005) |
| | | | Medium density fiberboard sawdust, Density 950 to 990 kg/m ³ , Particle size 150 to 850 micron, | Gan et al. (2004) |
| | | 95% NO ₃ -N removal; | D<2mm | Kim et al.(2000) |
| 4 | Wheat straw | | | Tshabalala (2002), Rocca et al. (2005) |
| | | 95% NO ₃ -N removal; | D<4mm | Kim et al.(2000) |
| 5 | Wood chips/Wood fibers | | D = 4.0 mm | Seelsaen et al. (2006) |
| | | 95% NO ₃ -N removal; | D<2mm | Kim et al.(2000) |
| | | Polynuclear Aromatic Hydrocarbons | Aspen wood fibers composed of 51% cellulose, 26% hemicellulose, 21% lignin, and 1% ash | Boving and Zhang (2002) |

| | | | | |
|---|------|--|--|---|
| | | | | Jokela et al. (2002), Savage and Tyrrel (2005) |
| 6 | Peat | Cu, Zn, Ni, PAHs (Polyaromatic hydrocarbons) | | DeBusk et. al. (1997), Clark and Pitt (1999), Clark et al. (2001), Kietlińska and Renman (2005) |

Table 2: Sorption media derived from sand and clay used to remove nutrients from storm water or wastewater

| No. | Sorption media | Additional environmental benefits in terms of removal | Physical/Chemical Properties | References |
|-----|------------------------------------|---|---|--|
| 1 | Sandy clay loam (SCL) | NO ₂ -N removal is 94%; NO ₃ -N removal is 90%; | Sand (53.28%), Silt (24.0%), Clay (22.72%); Porosity 0.51 | Güngör and Ünlü (2005) |
| 2 | Loamy sand (LS) | NO ₂ -N removal is 95%; NO ₃ -N removal is 93%; | Sand (78.28%), Silt (10.64%), Clay (11.08%); Porosity 0.33 | Güngör and Ünlü (2005) |
| 3 | Sandy loam (SL) | NO ₂ -N removal is 96%; NO ₃ -N removal is 73%; | Sand (70.28%), Silt (14.64%), Clay (15.08%); Porosity 0.45 | Güngör and Ünlü (2005) |
| 4 | Carbon sand, enretech sand or sand | | | Bell et al. (1995), DeBusk et al. (1997), Clark and Pitt (1999), Clark et al. (2001), Seelsaen et al. (2006) |
| 5 | Clay | Thiocyanates, Cadmium, Lead, Nickle | | Harris et al. (1996), Gálvez et al. (2003), Lazaridis (2003) |
| 6 | Zeolite+ Clay | | | GISVOLD et al. (2000) |
| 7 | Masonry sand | | Bulk density of masonry sand is 1670 kg/m ³ ; Porosity of masonry sand is 0.304. | Forbes et al. (2005) |
| 8 | Waste foundry sand | TCE, Zn, Metolachlor, Alachlor, | | Benson (2001) |

Table 3: Sorption media derived from minerals used to remove nutrients from storm water or wastewater

| No. | Sorption media | Additional environmental benefits | Physical/Chemical Properties | References |
|-----|----------------|-----------------------------------|------------------------------|--|
| 1 | Zeolites | Benzene, Sulfate, Chromate | | Clark and Pitt (1999), Li (2003), Seelsaen et al. (2006) |
| 2 | Perlite | | | Redco II (2007) |
| 3 | Opoka | | | Braun-Howland (2003) |

| | | | | |
|----|----------------|---------------------------------|---|---|
| 4 | Wollastonite | | | DeBusk et al. (1997), Hedström (2006) |
| 5 | Iron Sulfide | | | Tesoriero et al. (2000), Baeseman et al. (2006) |
| 6 | Limerock | | | DeBusk et al. (1997) |
| 7 | Allophane | | Clay-sized mineral containing silica, alumina and water | AEC (2007) |
| 8 | Chitin | | A natural polymer, technically known as polyacetylglucosamine | AEC (2007) |
| 9 | Pumice | | A light, porous volcanic rock composed of iron (18.2 %), aluminum (13.7%), calcium (12.7%) and magnesium (7.3%) and other. | AEC (2007) |
| 10 | Bentonite | | Montmorillonite mineral with about 4%-8% calcium carbonate, | AEC (2007) |
| | | | | Hedström (2006) |
| 11 | Clinoptilolite | | Density 55 lb/ft ³ ; Particle size 0.3 to 4.76 mm. | Smith et al. (2008) |
| 12 | Polonite | Zn, Ni, Co, Mn, Cu, Ba, Fe, Ti, | Manufactured from cretaceous rock Opoka (SiO ₂ 39.4%, CaO 42%, Al ₂ O ₃ 4.3%, Fe ₂ O ₃ 2.0%) | Kietlińska and Renman (2005) |
| 13 | Expanded shale | | Expanded shale (SiO ₂ 62.06%, Al ₂ O ₃ 15.86%, Fe ₂ O ₃ 5.80%, CaO 1.44%, MgO 1.68%); Bulk density of expanded shale is 728 kg/m ³ ; Porosity of expanded shale is 0.594; | Forbes et al. (2005) |
| | | | with sulfur, D= 2.38 to 4.76 mm | Zhang (2002) |
| 14 | Limestone | | D =2.38 to 4.76 mm | Darbi et al. (2002), Sengupta and Ergas (2006) |
| | | | D= 0.6 to 1.18 mm | Kim et al. (2000) |
| | | | Large particles 2 to 2.36 mm and small particles 0.6 to 1.18 mm | Kim et al.(2000) |
| 15 | Sulfur | | D =2.38 to 4.76 mm | Darbi et al. (2002) |

Table 4: Sorption media derived from waste materials used to remove nutrients from storm water or wastewater

| No. | Sorption media | Additional environmental benefits in terms of removal | Physical/Chemical Properties | References |
|-----|----------------|---|--|------------------------|
| | | 100% NO ₃ -N removal; | D (average)<4mm | Kim et al.(2000) |
| 1 | Newspaper | | 0.4 cm width ribbons, (25.49% extractives (protein, hemicellulose, labile carbon), 43.11% cellulose, 29.59% lignin, 2.59% ash) | Volokite et al. (1996) |

| | | | | |
|----|----------------------------|---|---|------------------------------|
| | | | Powder form, 28% Calcium, Average particle size 200 micron, Surface area 237 m ² /g, | Namasivayam et al. (2005) |
| 2 | Oyster shell | | | Sengupta and Ergas (2006) |
| 3 | Marbel chips | | Mg(OH) ₂ and CaCO ₃ | Sengupta and Ergas (2006) |
| 4 | Activated carbon | Cu, Fe, Pb, Zn | | Clark et al. (2001) |
| 5 | Tire crumb/Tire chips | 2,4-dichlorophenol (DCP), 4-chlorophenol (CP) | 20 to 40 mm, | Shin et al. (1999) |
| | | VOC | | Lisi et al. (2004), |
| 6 | Cotton waste | | | Rocca et. al. (2005) |
| 7 | Polyurethane porous media | | Porous structure, Average diameter 3-5 mm, External pore diameter 300 micron. | Han et al. (2001) |
| 8 | Blast furnace slage | | | Hedström (2006) |
| | | Zn, Ni, Co, Cu, Ba, | SiO ₂ 36.2%, CaO 35%, MgO 13.4%, Al ₂ O ₃ 10.6%, | Kietlińska and Renman (2005) |
| 9 | Oversized pulverozed brick | | | Savage and Tyrrel (2005) |
| 10 | Polystyrene packing | | | Savage and Tyrrel (2005) |
| 11 | Glass | | D= 4.0 mm | Seelsaen et al. (2006) |
| 12 | Lignocellulosic material | | Basically pine bark chips, | Tshabalala (2002) |

MATERIALS AND METHODS

Material Characterization

The research team screened the possible sorption media through the following five criteria: 1) the relevance of denitrification process, 2) the removal efficiency as evidenced in the literature with regard to adsorption, 3) the cost level, 4) the availability, 5) low maintenance and 6) additional environmental benefits. Four sorption media were eventually selected for final consideration according to a multi-criteria decision making (MCDM) process. They include sawdust/wood chip, paper/newspaper, tire crumb and astatula sand (citrus grove sand). The two media mixes selected for use in the column tests are denoted as recipe - 1 which consists of 68%

fine sand, 25% tire crumb, and 7% sawdust, and recipe - 2 which is composed of 69% fine sand, 25% tire crumb, and 6% paper/newspaper (by volume). The reason for using paper in recipe 2 to replace sawdust in recipe 1 is that the electron donor to triggering the denitrification process has to be present in the media by some way. At the end of the column tests, recipe 1 was further used for isotherm study and also as a media blend for microcosm system study.

The ASTM D-421-85 Standard Practice for Dry Preparation of Soil Samples for Particle-Size Analysis and Determination of Soil Constants was used. The Multi-point BET specific surface area by nitrogen adsorption method with respect to each type of recipe independently were performed by Quantachrome Instruments, which generated the surface area for these two mixed recipes as an average in the end. ASTM C29/C29M-07 - was applied for measuring the bulk density ("unit weight") and voids in soil and mixed media. ASTM D-854-92 Standard Test Method for Specific Gravity of Soils was applied for the determination of the specific gravity of soils and media that pass the 4.75-mm (No. 4) sieve.

Column Study

A laboratory column test method is a physical model, which attempts to simulate, on a small scale, a portion of the real world subsurface environment under a controlled set of experimental conditions. Lab column tests were conducted using three (2) plexi-glass columns (0.29 m inner diameter; 1.5 m height) with recipe - 1 and recipe - 2 respectively. The columns were packed in 5 cm lifts by adding pre-weighed dry sample. The final column porosity for both the columns was approximately 40%. For sampling ports, the columns were drilled holes at 1.37 m (4.5 ft) from top of the media as shown in Figure 1. Ball valves were used at the sampling ports and they were water sealed. The composition of all the columns in terms of weight and volume were thus determined as shown in Table 5. The feed solution (raw wastewater) from a functioning septic

tank in Orlando, Florida was stored and was used in the column study. Raw wastewater was pumped at the top of the columns as a continuous system. The columns were covered with a lid from top and bottom and the discharge ports were air tight so as to prevent direct contact of air thereby keeping the columns anoxic in condition. Sampling Method: Effluent samples were directly collected from the bottom of the columns at the sampling port. The sampling ports used were air tight ball valves. The ball valves were opened and effluent samples were extracted. The influent and effluent samples were collected in sterilized plastic bottles and were transported for water quality analysis to ERD lab.

Table 5: Composition of Columns in Terms of Weight and Volume

| | <i>Column STS</i> | | <i>Column STP</i> | |
|---------------|-------------------|--------------|-------------------|--------------|
| | <i>wt %</i> | <i>vol %</i> | <i>wt %</i> | <i>vol %</i> |
| Tire Crumb | 10.9 | 25.0 | 10.7 | 25.0 |
| Paper | - | - | 4.0 | 6.2 |
| Sawdust | 4.0 | 7.1 | - | - |
| Astatula Sand | 85.1 | 67.9 | 85.3 | 68.8 |

* Note: STS is the acronym of Sand, Tire Crum and Sawdust; STP is the acronym of Sand, Tire Crum and Paper

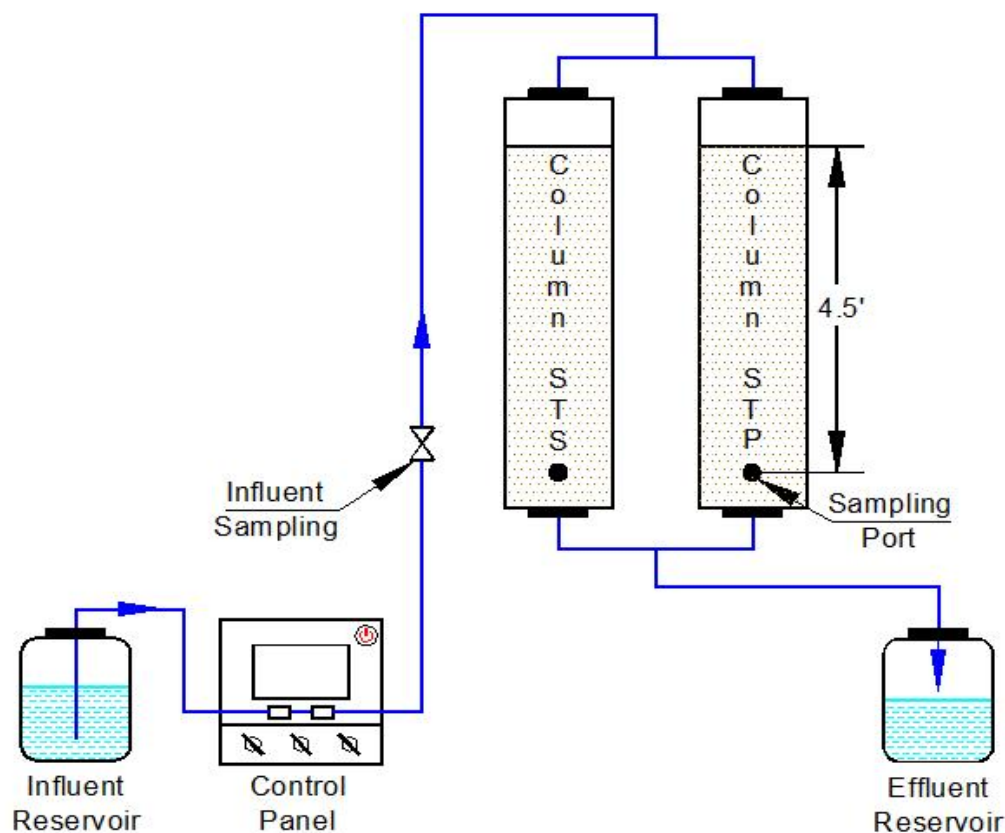


Figure 1: Schematic of Column Test

Batch Study

An Isotherm study as a batch process was carried out with recipe - 1 so as to study the sorption of ortho-phosphorus and nitrates. It is helpful in determining the sorption capacity and also the estimated life of the media for the sorption of nutrients. For isotherm study of nitrates, five flasks were prepared containing 100 gm of recipe - 1 and nitrate solution of 50 mL of 9.6, 8.4, 7.2, 6.0, 4.8 mg/L $\text{NO}_3\text{-N}$ was added in different flasks. The media mix and the solution were mixed thoroughly and kept for a residence time of 24 hours. After 24 hours, nitrate solution was extracted from the media and analyzed. For isotherm study of ortho-phosphates, one flask

was prepared containing 200 gm of recipe - 1 and phosphate solution of 100 mL of 4.12 mg/L $\text{PO}_4\text{-P}$. The media mix and the solution was mixed thoroughly and kept for a residence time of 24 hours. After 24 hours, phosphate solution was extracted from the media and analyzed. Using the same media mix in the flask 100 ml of fresh 4.12 mg/L $\text{PO}_4\text{-P}$ was added to the flask and mixed thoroughly and resided for 24 hours. The previous step was repeated for 6 days using the same media mix and the extracted solutions from the media were analyzed.

Microcosm Study

A Microcosm model is a small, representative system having analogies to a larger system in constitution, configuration and development. A microcosm model was built with a rectangular plastic container (L = 56 cm; W = 34.5 cm; D = 15 cm). The model mainly consists of two zones, treatment zone to the length of 46 cm whereas collection zone of 10 cm. Figure 2 shows the schematic of this system.

The bottom 5cm of the treatment zone consists of recipe - 1 whereas the rest of the model is packed with astatula sand. Synthetic wastewater flows into the model through the perforated tubing (inner diameter 0.3 cm) which acts as header pipes and has a downward slope of around 1%. These tubes are engineered with holes and slots, allowing it to collect and disperse the wastewater as it passes over the corrugations in the tubes. As the wastewater is distributed throughout the tubes, it trickles down to the media allowing partial biological breakdown before reaching the media. The wastewater is retained in the media for a hydraulic retention time of 72 hrs so as to provide the desired denitrification. The wastewater is retained in the treatment zone with the help of pre-fabricated riser at around 46 cm length and 6.5 cm in height as shown in Figure 2. The model is run as a continuous system and effluent is collected from the collection

zone. Additionally, the locations of sampling ports in the different compartments of the model are also depicted in Figure 2.

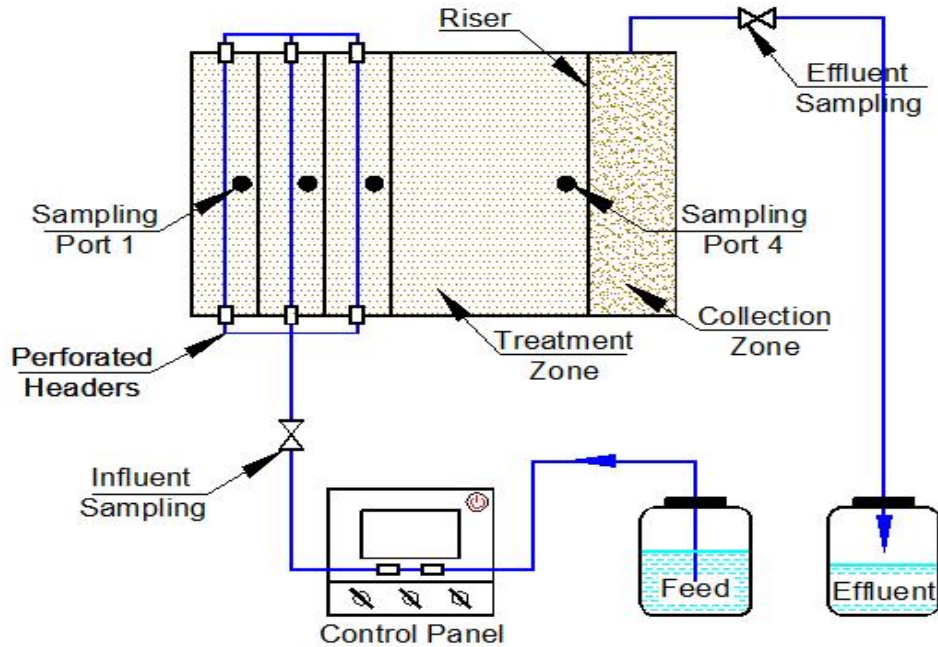


Figure 2: Experimental Design of Microcosm Model

RESULTS & DISCUSSION

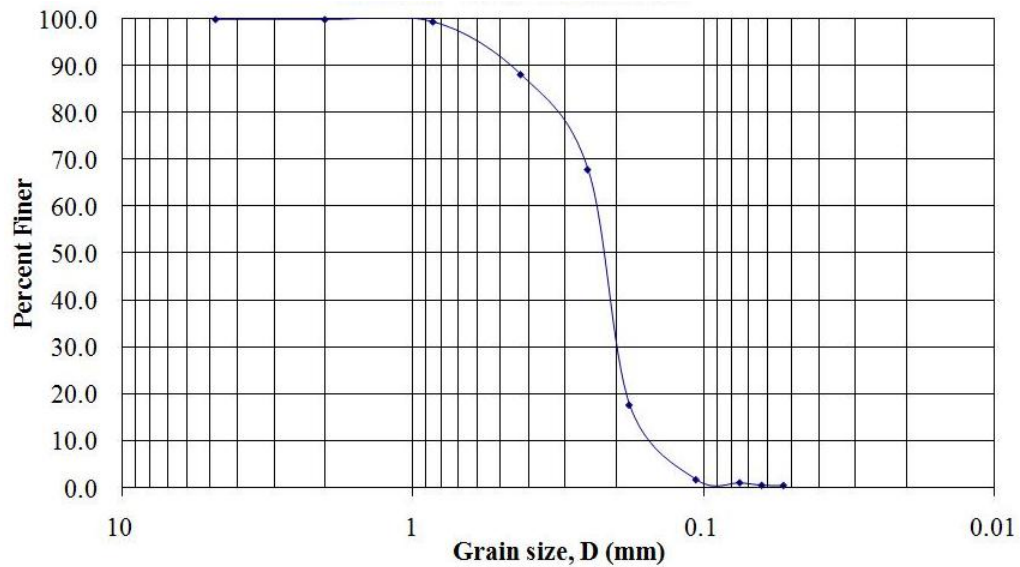
Material Characterization

The permeability of the astatula sand was measured to be 55.0 cm/hr (21.6 in/hr). The permeability of recipe 1 and recipe 2 were measured to be 54.4 cm/hr (21.4 in/hr) and 59.4 cm/hr (23.4 in/hr), respectively. To determine the particle-size distribution a sieve analysis was performed. Table 6 lists the summary of material characterization of the astatula sand and the two recipes used for the column tests. Surface area of astatula sand, recipe – 1 and recipe – 2 are approximately $0.32 \text{ m}^2 \text{ g}^{-1}$, $0.08 \text{ m}^2 \text{ g}^{-1}$ and $0.18 \text{ m}^2 \text{ g}^{-1}$ respectively. Surface areas were

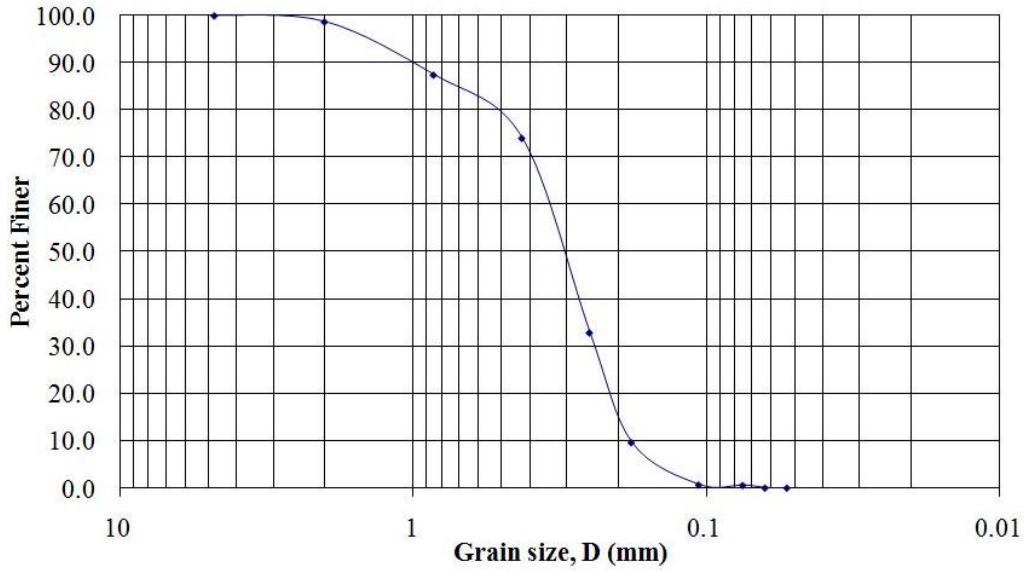
determined by a nitrogen sorption BET test (Quantachrome Instruments, Boynton Beach, FL). Figure 3(a), 3(b), and 3(c) present the gradation curve of Astatula sand and two mixes used in our recipes comparatively.

Table 6: Summary of Material Characterization

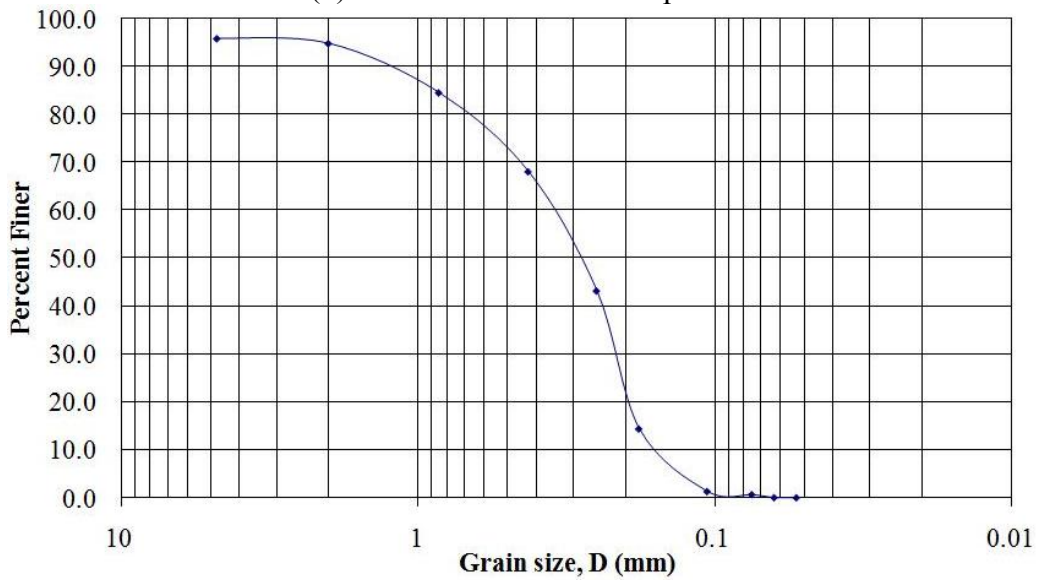
| | <i>Astatula Sand</i> | <i>Recipe - 1</i> | <i>Recipe - 2</i> |
|--|----------------------|-------------------|-------------------|
| Density (g cc ⁻¹) | 1.53 | 1.24 | 1.28 |
| Void Ratio (unit less) | 0.73 | 0.69 | 0.62 |
| Porosity (unit less) | 0.42 | 0.41 | 0.38 |
| Specific Gravity (Gs) | 2.65 | 2.32 | 2.15 |
| Surface Area (m ² g ⁻¹) | 0.32 | 0.08 | 0.18 |
| Permeability (cm hr ⁻¹) | 55.0 | 54.4 | 59.4 |



(a) Gradation curve of Astatula Sand



(b) Gradation curve of Recipe - 1



(c) Gradation curve of Recipe - 2

Figure 3: Gradation curve of natural soil and sorption media

Column Study

The following Table 7 presents the results from the Column Study for Column STS and Column STP with Recipe 1 and Recipe 2 respectively. During the experimental period the columns did not show any signs of saturation with nutrients although the columns were loaded with high concentrations of nutrients with average total phosphorus concentration of 188 mg/L

which is approximately thirteen fold than the average concentration of 14 mg/L for total phosphorus (USEPA, 2002) and average total nitrogen concentration of 415 mg/L which is approximately eight fold than the average concentration of 50 mg/L for total nitrogen (USEPA, 2002).

Table 7: Results from Column Study in 2006-2007 time period

| | 19-Oct | 26-Oct | 10-Nov | 17-Nov | 30-Nov | 2-Feb | 26-Feb | 7-Mar | Avg Conc [mg/L] |
|---|--------|--------|--------|--------|--------|-------|--------|-------|--------------------|
| <i>Nitrates</i> | | | | | | | | | |
| Influent | 0.27 | 0.31 | 3.02 | 3.49 | 3.10 | 0.16 | 0.21 | 1.95 | 1.56 |
| Recipe 1 | 0.04 | 0.06 | 0.08 | 0.02 | 0.15 | 0.01 | 0.01 | 0.02 | 0.05 |
| Recipe 2 | 0.03 | 0.06 | 0.11 | 0.08 | 0.86 | 0.08 | 0.01 | 0.03 | 0.16 |
| Average Percentage Removal (%); Recipe 1 = 97.0 & Recipe 2 = 90.1 | | | | | | | | | |
| <i>Ammonia</i> | | | | | | | | | |
| Influent | 4.9 | 27.8 | 1.5 | 119 | 112 | 10.7 | 72.9 | - | 49.7 |
| Recipe 1 | 0.3 | 3.7 | 0.7 | 4.1 | 4.4 | 6.7 | 10.8 | - | 4.4 |
| Recipe 2 | 0.1 | 0.2 | 0.0 | 0.1 | 0.8 | 0.9 | 11.0 | - | 1.9 |
| Average Percentage Removal (%); Recipe 1 = 91.2 & Recipe 2 = 96.2 | | | | | | | | | |
| <i>Total Nitrogen</i> | | | | | | | | | |
| Influent | 96.4 | 35.6 | 1135 | 488 | 689 | 678 | 126 | 67.5 | 414 |
| Recipe 1 | 6.2 | 6.4 | 5.3 | 4.2 | 5.2 | 6.9 | 12.1 | 10.3 | 7.1 |
| Recipe 2 | 5.1 | 7.0 | 6.5 | 5.7 | 5.4 | 1.1 | 15.9 | 0.9 | 6.0 |
| Average Percentage Removal (%); Recipe 1 = 98.3 & Recipe 2 = 98.6 | | | | | | | | | |
| <i>Ortho Phosphorus</i> | | | | | | | | | |
| Influent | 0.86 | 0.91 | 0.81 | 0.63 | 0.73 | 0.23 | 0.71 | 1.26 | 0.77 |
| Recipe 1 | 0.01 | 0.00 | 0.02 | 0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 |
| Recipe 2 | 0.02 | 0.01 | 0.02 | 0.02 | 0.01 | 0.01 | 0.05 | 0.00 | 0.02 |
| Average Percentage Removal (%); Recipe 1 = 98.8 & Recipe 2 = 97.8 | | | | | | | | | |
| <i>Total Phosphorus</i> | | | | | | | | | |
| Influent | 6.8 | 4.2 | 705 | 195 | 550 | 36.1 | 3.2 | 2.1 | 188 |
| Recipe 1 | 0.15 | 0.06 | 0.23 | 0.09 | 0.18 | 0.09 | 0.08 | 0.14 | 0.13 |
| Recipe 2 | 0.21 | 0.08 | 0.19 | 0.15 | 0.21 | 0.19 | 0.07 | 0.07 | 0.15 |
| Average Percentage Removal (%); Recipe 1 = 99.9 & Recipe 2 = 99.9 | | | | | | | | | |

BOD

| | | | | | | | | | |
|---|---|---|------|------|------|------|------|------|------|
| Influent | - | - | 2180 | 1475 | 7200 | 606 | 173 | 198 | 1972 |
| Recipe 1 | - | - | 240 | 45.0 | 405 | 85.0 | 36.9 | 52.0 | 144 |
| Recipe 2 | - | - | 751 | 750 | 833 | 342 | 2.00 | 48.0 | 454 |
| Average Percentage Removal (%); Recipe 1 = 92.7 & Recipe 2 = 76.7 | | | | | | | | | |

In the previous study by Davis et al. (2003), paper and sawdust showed some excellent results in terms of nitrate removal and were accepted as one of the best electron donors. In this research, sawdust and paper (newspaper) showed similar results and were just not limited to nitrates but also to total nitrogen, total phosphorus, ammonia, ortho-phosphorus and BOD. At the end of the experimental period, the newspaper print in the columns was still visible and most of the newspaper in the media mix remained similar in appearance to the original material. These observations are consistent with other studies that indicate that newspaper is somewhat resistant to bacterial degradation under anoxic conditions (Cummings and Stewart, 1994; Volokita et al, 1996; Davis et al, 2003). This resistance seems to be the chemical composition of newspaper, in particular the relatively high lignin content. Tire crumb that was used for this research has carbon content of 85% and does not have any metal content. Though tire crumb was never used as an individual media for the septic tank drainfield, the results indicate that it has a strong potential for creating an environmentally safe and value-added option for scrap tire reuse.

Overall, the green sorption media showed significant potential for pollutant removal in a septic tank drainfield. Throughout the experimental period, both the columns showed almost equal and consistent removal of more than 90% for all the water quality parameters (i.e., ortho-phosphorus, total phosphorus, nitrates, total nitrogen, ammonia, BOD).

Batch Study

The results for the nitrate and ortho-phosphate isotherm results are presented in Table 8(a) and 4(b) respectively. It can be seen from Table 4(a) that there is very little or no removal of

nitrates. It was concluded that the nitrates was not sorbed by the sorption media and biological activity could not initiate as the batch studies were performed in 24 hrs. However, substantial removal of phosphorus was observed from the batch tests. The sorption results for phosphorus were plotted for the linearized form of Langmuir and Freundlich Isotherm Model as shown in Figure 4(a) and 4(b) respectively. The linearized form of Langmuir and Freundlich isotherm models are as presented below:

Table 8: Isotherm Results

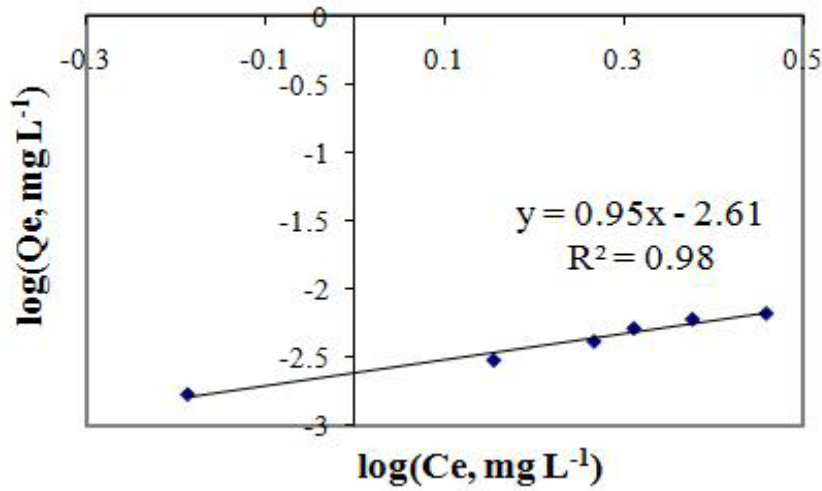
| (a) Nitrate Isotherm Results | | | (b) Phosphate Isotherm Results | | |
|------------------------------|--------------------------|--------------------------|--------------------------------|--------------------------|--------------------------|
| <i>Sample</i> | <i>Mass Loading [mg]</i> | <i>Mass Removed [mg]</i> | <i>Sample</i> | <i>Mass Loading [mg]</i> | <i>Mass Removed [mg]</i> |
| 1 | 0.48 | 0.11 | 1 | 0.41 | 0.35 |
| 2 | 0.42 | 0.00 | 2 | 0.41 | 0.27 |
| 3 | 0.36 | 0.08 | 3 | 0.41 | 0.23 |
| 4 | 0.30 | 0.01 | 4 | 0.41 | 0.21 |
| 5 | 0.24 | 0.00 | 5 | 0.41 | 0.17 |
| | | | 6 | 0.41 | 0.12 |

Langmuir isotherm equation: $(1/Q_e) = (1/(Q_{max}b)) \times (1/C_e) + (1/Q_{max}) \dots\dots\dots$ (Eq. 1)

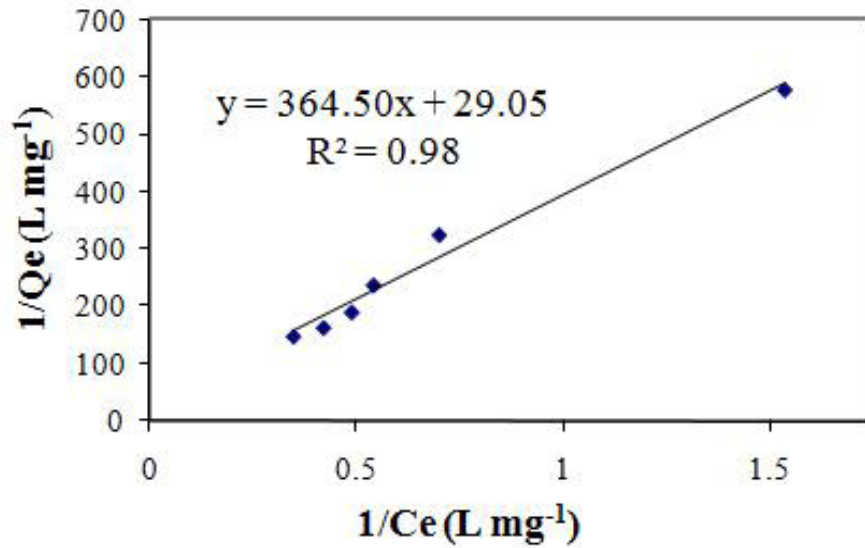
where: Q_e = Sorbed concentration [mass adsorbate/mass adsorbent]; Q_{max} = Maximum capacity of adsorbent for adsorbate [mass adsorbate/mass adsorbent]; b = Measure of affinity of adsorbate for adsorbent; C_e = Aqueous concentration of adsorbate [mass/volume].

Freundlich isotherm equation: $\log q_e = \log K + (1/n) \log C_e \dots\dots\dots$ (Eq. 2)

where: q_e = Sorbed concentration [mass adsorbate/mass adsorbent]; K = Capacity adsorbent [mass adsorbate/mass adsorbent]; C_e = Aqueous concentration of adsorbate [mass/volume]; n = Measure of how affinity for the adsorbate changes with changes in adsorption density.



(a) Freundlich Plot



(b) Langmuir Plot

Figure 4: Isotherm Plots

Assume that monolayer coverage of phosphorus adsorbed to the media surface. From the graphical plots as shown in Figure 4(a) and 4(b), the adsorption capacity for phosphorus from the Langmuir and Freundlich isotherm models were calculated to be 34.4 mg g^{-1} and 0 mg g^{-1}

respectively. It can be concluded that the Langmuir Equation fits better for the sorption of phosphorus.

Microcosm Study

The results from the Microcosm model are as presented in Table 9. The samples illustrated around 80% removal efficiency for nitrates and ortho-phosphorus. Additionally, the results also include the concentration and removal efficiency from sampling ports located in the different compartment of the model. It appears that most of the denitrification reactions occur in the last compartment before riser in the microcosm in which a well fostered anoxic environment can be maintained throughout the operation. This observation is consistent with our design philosophy completely.

Table 9: Results from Microcosm Model

| | <i>Nitrates</i> | | | <i>Ortho-Phosphorus</i> | | |
|-----------------|---------------------------------------|----------------------------|--------------------------------|---------------------------------------|----------------------------|--------------------------------|
| | <i>Concentration</i> <i>[mg/L]</i> | <i>%</i> <i>Removal</i> | <i>Cum %</i> <i>Removal</i> | <i>Concentration</i> <i>[mg/L]</i> | <i>%</i> <i>Removal</i> | <i>Cum %</i> <i>Removal</i> |
| Influent | 2.38 | | | 1.28 | | |
| Sampling Port 1 | 2.33 | 1.87 | 1.87 | 1.15 | 10.17 | 10.17 |
| Sampling Port 2 | 2.26 | 2.91 | 4.79 | 1.02 | 10.67 | 20.84 |
| Sampling Port 3 | 1.72 | 22.68 | 27.47 | 0.76 | 20.33 | 41.17 |
| Sampling Port 4 | 0.49 | 52.03 | 79.50 | 0.23 | 40.91 | 82.08 |
| Effluent | 0.47 | 0.62 | 80.12 | 0.20 | 2.16 | 84.24 |

To determine the life of the green sorption media, which is applied as a 5 cm (2 inch) layer in the microcosm model, only two factors need to be known. These factors are the mass of the pollution control media and the phosphate mass loading rate per year. Knowing that the density of the green sorption media is 1.37 g cc⁻¹ (85.5 lbs ft⁻³), the mass of media is 11,719 grams. Also knowing that the average concentration of phosphorus coming into the drainfield is around 14 mg L⁻¹ (<http://pubs.usgs.gov/sir/2004/5299>: USEPA, 2002) and daily flow of wastewater to the

model is 1.25 L, the mass loading of phosphate year is determined to be about 6,388 mg yr⁻¹. Additionally, the adsorption capacity from the batch isotherm tests for phosphorus was estimated to be around 34.4 mg g⁻¹. The life of the green sorption media is thereby calculated to be about 63 years.

CONCLUSION

The information generated in the present study is valuable for understanding the postulated development of green sorption media applied to solve the nutrient removal in an innovative septic tank underground drainfield. Under the hydraulic retention time (HRT) of 24 hours, samples illustrated treatment efficiencies of greater than 90% for both the columns for all pollutants of concerns. The batch adsorption isotherm data was fitted in the Langmuir isotherm and Freundlich isotherm models, and adsorption capacity for phosphorus was found to be 34.4 mg g⁻¹ based on Langmuir isotherm. A microcosm of the septic tank underground drainfield was built with one of the recipes applied in the column test as a continuous system dosed with synthetic wastewater. Under the HRT of 72 hours, samples from the microcosm physical model illustrated more than 80% of removal efficiency for nitrates and phosphorus. Additionally, with the aid of the isotherm tests, the life expectancy of the proposed sorption media in the microcosm physical model was estimated to be around 63 years for phosphorus sorption. The significant removal efficiencies of the targeted contaminants suggest that the use of such green sorption media might be a suitable and powerful material for an *in-situ* remediation of nitrate and ortho-phosphate contaminated in groundwater. Overall, this research demonstrates the effectiveness of sawdust and paper as electron donors in a drainfield whereas tire crumb may have better adsorption capacity for nutrient removal. The field study in the future would be more

appropriate to examine the long-term performance and determine the expected life of the media mix in terms of removal of nutrients. Economic analysis is also planned to be carried out so as to compare the new drainfield against the conventional standard drainfield.

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